

# On DLA's $\eta$

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## 1 SUMMARY

2 In his pioneering paper on seismic anisotropy in a layered earth, Anderson (1961) introduced a  
3 parameter often referred in global seismology as  $\eta$  without providing any reasoning. This note  
4 hopes to clarify the significance of  $\eta$  in the context of the dependence of bodywave velocities in  
5 a transversely isotropic system on the angle of incidence, and also its relation with the other  
6 well-known anisotropic parameters introduced by Thomsen (1986).

7 **Key words:** Seismic anisotropy, transverse isotropy, radial anisotropy.

## 8 Introduction

9 To describe a radially anisotropy (transversely isotropy with a vertical symmetry axis, VTI)  
10 system, we employ the Love's original notation (Love, 1927), where stress and strain tensors  
11 are related by

$$\begin{bmatrix} \tau_{11} \\ \tau_{22} \\ \tau_{33} \\ \tau_{23} \\ \tau_{31} \\ \tau_{12} \end{bmatrix} = \begin{bmatrix} A & H & F & & & \\ & H & A & F & & \\ & F & F & C & & \\ & & & & L & \\ & & & & & L \\ & & & & & & N \end{bmatrix} \begin{bmatrix} e_{11} \\ e_{22} \\ e_{33} \\ 2e_{23} \\ 2e_{31} \\ 2e_{12} \end{bmatrix} \quad (1)$$

12 where  $H = A - 2N$ . There are five independent parameters,  $A$ ,  $C$ ,  $F$ ,  $L$ ,  $N$ , to describe this  
13 system, while there are two,  $\lambda$ ,  $\mu$ , for the isotropic case, for which  $A = C = \lambda + 2\mu$ ,  $F = \lambda$ ,  
14  $L = N = \mu$ . For convenience, Anderson (1961) introduced the following "anisotropy factors":

$$\varphi = C/A = \alpha_V^2/\alpha_H^2 \quad (2)$$

$$\xi = (A - H)/2L = N/L = \beta_H^2/\beta_V^2 \quad (3)$$

$$\eta = (A - 2L)/F, \quad (4)$$

15 which are all equal to 1 for isotropic case ( $\alpha_V = \sqrt{C/\rho}$ ,  $\alpha_H = \sqrt{A/\rho}$ ,  $\beta_H = \sqrt{N/\rho}$ ,  $\beta_V =$   
16  $\sqrt{L/\rho}$ , where  $\rho$  gives the density.).

17 While both  $\varphi$  and  $\xi$  have simple meanings (degree of anisotropy in P- and S-wave, re-  
 18 spectively), the physical meaning of  $\eta$  is not so trivial. Takeuchi and Saito (1972), in their  
 19 monograph on seismic surface waves, reversed the order of the denominator and numerator in  
 20 the definition of  $\eta$  as,

$$\eta = F/(A - 2L), \quad (5)$$

21 without commenting on the physical meaning either. As the expression of Takeuchi and Saito  
 22 (1972) is now commonly used in the global seismological community, we will use this notation  
 23 and denote it as  $\eta_{DLA} = F/(A - 2L)$  in the following. In his text book, Anderson (1989) called  
 24 this  $\eta_{DLA}$  “the fifth parameter required to fully describe transverse isotropy”. In Dziewonski  
 25 and Anderson (1981), by showing examples, the effect of  $\eta_{DLA}$  on the incident angle dependence  
 26 of the phase velocity of P and S waves is discussed, and we generally think that  $\eta_{DLA}$  controls,  
 27 to some extent, the incidence angle dependence of those bodywaves, as well as those of Rayleigh  
 28 waves.

29 The purpose of this short note is provide simple theoretical background to how  $\eta_{DLA}$  affects  
 30 the bodywave propagation.

### 31 Incidence angle dependence of bodywaves

32 By solving an eigenvalue problem of an appropriate Christoffel matrix, the incident angle,  $\theta$   
 33 dependence of bodywave phase velocities can be obtained as

$$\rho v_P^2(\theta) = \frac{(L + C) + (A - C) \sin^2 \theta + \sqrt{S}}{2} \quad (6)$$

$$\rho v_{SV}^2(\theta) = \frac{(L + C) + (A - C) \sin^2 \theta - \sqrt{S}}{2} \quad (7)$$

$$\rho v_{SH}^2(\theta) = L + (N - L) \sin^2 \theta, \quad (8)$$

34 where  $v_P$ ,  $v_{SV}$ , and  $v_{SH}$  denote phase velocities of pseudo- P, SV and SH waves respectively,  
 35 and

$$S = \{(A - L) \sin^2 \theta - (C - L) \cos^2 \theta\}^2 + (F + L)^2 \sin^2 2\theta \quad (9)$$

$$= \{(A - L) \sin^2 \theta + (C - L) \cos^2 \theta\}^2 + \{(F + L)^2 - (C - L)(A - L)\} \sin^2 2\theta \quad (10)$$

$$= \{(C - L) + (A - C) \sin^2 \theta\}^2 + \{(F + L)^2 - (C - L)(A - L)\} \sin^2 2\theta \quad (11)$$

$$= (C - L)^2 + (A - C)(A + C - 2L) \sin^2 \theta + \{(F + L)^2 - (\frac{A + C}{2} - L)^2\} \sin^2 2\theta. \quad (12)$$

36 When the condition

$$(F + L)^2 = (C - L)(A - L) \quad (13)$$

is satisfied, equation (11) will be  $S = \{(C - L) + (A - C) \sin^2 \theta\}^2$ , and

$$\rho v_P^2(\theta) = C + (A - C) \sin^2 \theta \quad (14)$$

$$\rho v_{SV}^2(\theta) = L \quad (15)$$

$$\rho v_{SH}^2(\theta) = L + (N - L) \sin^2 \theta. \quad (16)$$

37 The condition (13) is called by Thomsen (1986) the elliptic condition, since, in the absence  
 38 of the  $\sin^2 2\theta$  term, the forms of the wave velocity surfaces as a function of incidence angle  $\theta$   
 39 are elliptical with only a  $\sin^2 \theta$  dependence. When condition (13) is not satisfied the presence  
 40 of the  $\sin^2 2\theta$  term means that the wavesurfaces can be either convex or concave. (The convex-  
 41 ity/concavity of the P velocity is in the opposite sense to that of the SV velocity. This is an  
 42 explicit consequence of the presence of the  $\sqrt{S}$  term in (6) and (7) with opposite signs.)

43 Thus if we were to introduce an additional parameter to characterize the incidence angle  
 44 dependence of bodywaves, one reasonable choice may be

$$\eta_\kappa = \frac{F + L}{(A - L)^{1/2}(C - L)^{1/2}}, \quad (17)$$

45 and  $\eta_\kappa = 1$  for the isotropic case.

46 Further considering

$$(A - L)(C - L) = \left(\frac{A + C}{2} - L\right)^2 - \left(\frac{A - C}{2}\right)^2,$$

47

$$\eta_{\kappa'} = \frac{F + L}{\frac{A + C}{2} - L} \quad (18)$$

48 may be another possibility that might make sense by looking at equation (12).

49 One of the good points of  $\eta_{DLA}$  is that it is simple and depends on just  $A$  and not  $C$ .  
 50 Assuming P-wave anisotropy is small, if we substitute  $\frac{A + C}{2}$  in (18) by  $A$ , we get

$$\eta_{\kappa''} = \frac{F + L}{A - L} \quad (19)$$

51 It is instructive how these parameters ( $\eta$ 's) behave when both P- and S-wave anisotropy is  
 52 absent (i.e.,  $A = C$  and  $L = N$ ). When these conditions are satisfied,

$$\begin{aligned} \rho v_P^2(\theta) &= \frac{(L + A) + \sqrt{S}}{2} \\ \rho v_{SV}^2(\theta) &= \frac{(L + A) - \sqrt{S}}{2} \\ \rho v_{SH}^2(\theta) &= L, \end{aligned}$$

53 and

$$S = \{(A - L)\}^2 + \{(F + L)^2 - (A - L)^2\} \sin^2 2\theta,$$

54 and  $\sin^2 \theta$  dependence disappears. In this case,  $\eta_\kappa$ ,  $\eta_{\kappa'}$ , and  $\eta_{\kappa''}$  reduce to the same form. Also,  
 55 it is easy to see that  $\eta_{DLA} = 1$  gives the elliptic condition, and so in this sense,  $\eta_{DLA} - 1$   
 56 becomes a measure of a departure from the elliptic condition to dictate the convex/concave  
 57 pattern.

58 For more general case,  $\chi = \eta_{DLA} - 1$  is small for weak anisotropy,

$$\chi = \eta_{DLA} - 1 = \frac{F - A + 2L}{A - 2L}. \quad (20)$$

59 Similarly

$$\chi'' = \eta_{\kappa''} - 1 = \frac{F - A + 2L}{A - L} = \chi \times \frac{A - 2L}{A - L}, \quad (21)$$

60 and as long as  $A - L > A - 2L > 0$  is satisfied,  $\chi''$  has the same sign as  $\chi$ , and  $\chi > \chi''$ , indicating  
 61  $\chi''$  is also small. So in this respect, if anisotropy is weak (especially in P),  $\eta_{DLA}$  might be a  
 62 good proxy for  $\eta_\kappa$  whose departure from unity provides a measures of the deviation from elliptic  
 63 anisotropy and dictates the convex/concave pattern of the incidence angle dependence of  $v_P$   
 64 and  $v_{SV}$ .

## 65 Thomsen's parameters

66 Thomsen (1986) introduced three parameters for VTI system, now referred to as Thomsen's  
67 parameters, and they are defined as

$$\varepsilon = \frac{A - C}{2C} = \frac{1}{2}(\varphi^{-1} - 1) \quad (22)$$

$$\gamma = \frac{N - L}{2L} = \frac{1}{2}(\xi - 1) \quad (23)$$

$$\delta = \frac{(F + L)^2 - (C - L)^2}{2C(C - L)}, \quad (24)$$

68 which are all small for weak anisotropy. While  $\varepsilon$  and  $\gamma$  are directly related to  $\varphi$  and  $\xi$  respec-  
69 tively as shown above and thus to P- and S-wave anisotropy,  $\delta$  was introduced such that it  
70 dominates  $v_P$  in the case of near vertical incidence as in reflection profiling.

71 Considering that  $\delta = \varepsilon$  is their condition for elliptical anisotropy, examination of  $\varepsilon - \delta$  leads  
72 to

$$\varepsilon - \delta = \frac{A - C}{2C} - \frac{(F + L)^2 - (C - L)^2}{2C(C - L)} \quad (25)$$

$$= \frac{(A - L)(C - L) - (F + L)^2}{2C(C - L)} \quad (26)$$

$$= (1 - \eta_\kappa^2) \frac{A - L}{2C}, \quad (27)$$

73 and we now see the connection between Thomsen's  $\delta$  and  $\eta_\kappa$  introduced here. If  $\eta_{DLA}$  were a  
74 proxy of  $\eta_\kappa$  for weak anisotropy, we might be able to say that a connection between  $\eta_{DLA}$  and  
75 Thomsen's  $\delta$  is established.

76 For weak anisotropy, the incidence angle dependence of bodywaves are, according to Thom-  
77 sen (1986),

$$v_P(\theta) = \alpha_H (1 + \delta \sin^2 \theta \cos^2 \theta + \varepsilon \sin^4 \theta) \quad (28)$$

$$v_{SV}(\theta) = \beta_V \left[ 1 + \frac{\alpha_H^2}{\beta_V^2} (\varepsilon - \delta) \sin^2 \theta \cos^2 \theta \right] \quad (29)$$

$$v_{SH}(\theta) = \beta_V (1 + \gamma \sin^2 \theta), \quad (30)$$

78 and when the elliptic condition is satisfied

$$v_P(\theta) = \alpha_H (1 + \varepsilon \sin^2 \theta)$$

$$v_{SV}(\theta) = \beta_V$$

$$v_{SH}(\theta) = \beta_V (1 + \gamma \sin^2 \theta),$$

79 which show simple incidence angle dependences.

80 (28)(29)(30) may be expressed in terms of  $2\theta$  and  $4\theta$  to make the incidence angle dependence  
81 more explicit:

$$v_P(\theta) = \alpha_H \left[ 1 + \frac{\varepsilon}{2}(1 - \cos 2\theta) - \frac{\omega}{2}(1 - \cos 4\theta) \right] \quad (31)$$

$$v_{SV}(\theta) = \beta_V \left[ 1 + \frac{\alpha_H^2 \omega}{\beta_V^2} \frac{\omega}{2}(1 - \cos 4\theta) \right] \quad (32)$$

$$v_{SH}(\theta) = \beta_V \left[ 1 + \frac{\gamma}{2}(1 - \cos 2\theta) \right], \quad (33)$$

82 where  $\omega = (\varepsilon - \delta)/4$  is introduced. These equations show that  $(\varepsilon - \delta)$  dictates the con-  
83 vex/concave nature (i.e,  $\cos 4\theta$  dependence) of  $v_P$  and  $v_{SV}$ .

84  $\eta_{DLA}$  and  $\eta_{\kappa}$  for weakly anisotropic models

85 To finish up this short note, we compare distributions of  $\eta$ -related parameters for some of  
 86 weakly anisotropic cases.

87 Millefeuille (isotropic layers) case

88 In the first example, we present a series of VTI models constructed by the Backus averaging  
 89 (Backus, 1962) of a stack of two kinds of homogeneous isotropic layers: soft layers embedded in  
 90 a background solid matrix (e.g., Kawakatsu et al., 2009). We parameterize (i) the proportional  
 91 reduction of rigidity of soft layers to the background by  $a$  ( $0 \leq a \leq 1$ ), (ii) the proportional  
 92 reduction of the bulk modulus by  $a/2$ , and (iii) the volume fraction of soft layers by  $f$  ( $0 \leq$   
 93  $f \leq 1$ ). Both  $a$  and  $f$  are varied in intervals of 0.05. Figure 1(a) compares  $\eta_{\kappa}$  with  $\eta_{DLA}$   
 94 (blue circles) or  $\eta_{\kappa'}$  (magenta crosses). While  $\eta_{\kappa}$  and  $\eta_{\kappa'}$  give almost the same values,  $\eta_{DLA}$

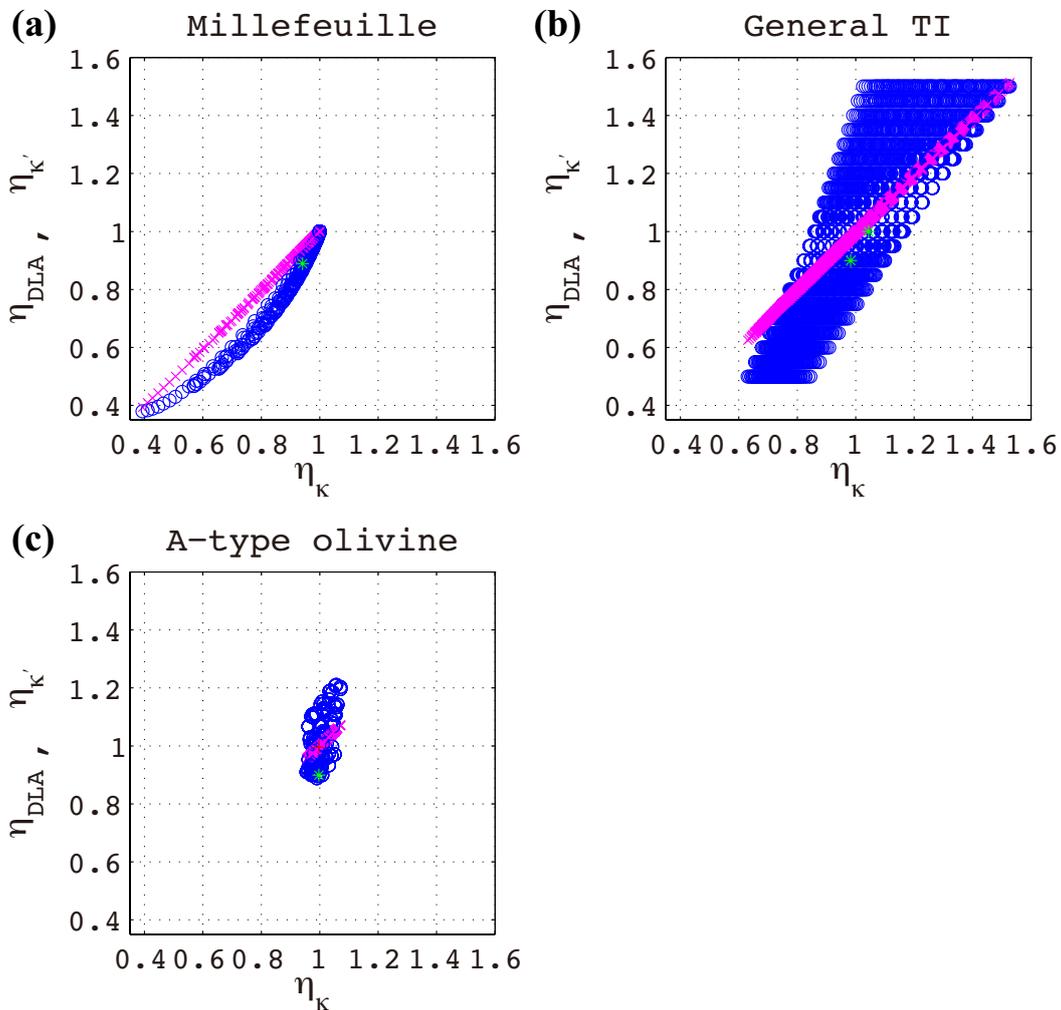


Figure 1: Comparison of  $\eta$ -related parameters for various weakly anisotropic models. (a) Millefeuille case, (b) general TI case, and (c) rotated A-type olivine case. Green asterisks correspond to  $\eta_{\kappa}$  vs.  $\eta_{DLA}$  for (a)  $a = 0.9$ ,  $f = 0.01$ , (b) peak-to-peak anisotropy for both P and S waves is 1.5% with  $\eta_{DLA} = 0.9$ , 1.0, and (c) the A-type olivine fabric case whose fast axis lies in the horizontal plane, all for which examples of incident angle dependency of bodywaves are shown in Figure 2.

95 gives slightly smaller values. As  $\eta_\kappa \leq 1$  is guaranteed (Berryman, 1979), all values appear  
96 generally less than 1. Although  $\eta_{DLA}$  in this case slightly deviates from  $\eta_\kappa$ , nearly one-to-one  
97 correspondence may be observed to make  $\eta_{DLA}$  a reasonable proxy to  $\eta_\kappa$ .

## 98 **General case**

99 For a more general case, we construct a series of VTI models which have a maximum of  $\pm 5\%$   
100 anisotropy in both  $\alpha_{V,H}$  and  $\beta_{V,H}$ , and  $0.5 < \eta_{DLA} < 1.5$  (Figure 1(b)). While  $\eta_\kappa$  and  $\eta_{\kappa'}$  give  
101 almost the same values,  $\eta_{DLA}$  deviates significantly from the corresponding  $\eta_\kappa$ .

## 102 **A-type olivine case**

103 As a third example, we construct a series of VTI models by azimuthal averaging (Montagner  
104 and Nataf, 1986; Montagner and Anderson, 1989) of an arbitrarily rotated A-type olivine fabric  
105 (Jung et al., 2006) (Figure 1(c)) (rotation is done with a 30-degree interval for each Euler angle).  
106 In a similar way to the preceding cases,  $\eta_\kappa$  and  $\eta_{\kappa'}$  have almost the same values, but  $\eta_{DLA}$   
107 deviates from corresponding  $\eta_\kappa$ .

108 Examples of the incidence angle dependence of representative VTI models (denoted by  
109 green asterisks in Figure 1) are shown in Figure 2. Note that the convex pattern of  $v_{SV}$   
110 velocity occurs when  $\eta_\kappa < 1$ .

## 111 **Discussion**

112 The incidence angle dependence of bodywave phase velocities in a radially anisotropic system  
113 has not been discussed much in the geophysical literature as it is a difficult effect to observe.  
114 In the laboratory, on the other hand, the simple  $\sin \theta$  and  $\sin 2\theta$  dependence (e.g., (6) and (11))  
115 has been used to obtain the fifth elastic constant from measurement along the angle 45 degrees  
116 from the symmetric axes (e.g., Christensen and Crosson, 1968; Anderson, 1966). Song and  
117 Kawakatsu (2012, 2013) recently suggested that such incident angle dependency in the Earth  
118 may be constrained at subduction zones where the dip of the lithosphere/asthenosphere changes  
119 along with the subduction, affecting the effective incidence angle of teleseismic bodywaves to  
120 the system. If such analyses can be made generally, the new parameter  $\eta_\kappa$  (or  $\eta_{\kappa'}$ ) might be  
121 a useful tool in global seismology to characterize VTI (radially anisotropic) systems. How  
122  $\eta$ -related parameters might be constrained from Rayleigh wave dispersion needs also to be  
123 understood (e.g., Anderson, 1966).

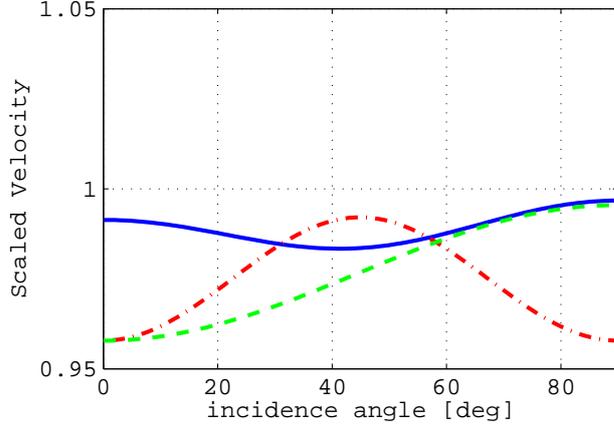
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129 robbed us of the opportunity to discuss with him directly how he came up with his  $\eta$ .

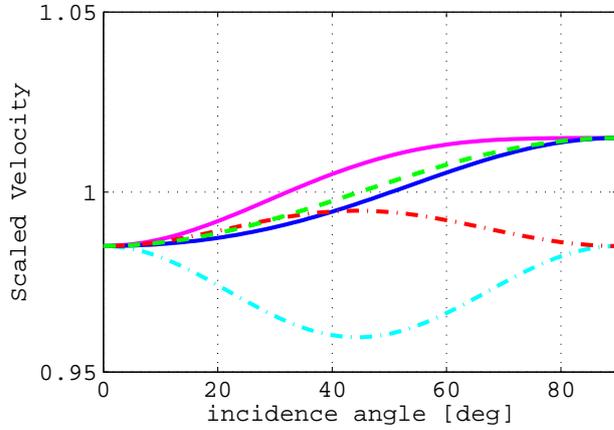
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MF,  $a = 0.9$ ,  $f = 0.01$ ,  $R_p = 0.54\%$ ,  $R_s = 3.9\%$ ,  $\eta_{DLA} = 0.889$ ,  $\eta_\kappa = 0.941$



GE,  $R_p = 3\%$ ,  $R_s = 3\%$ ,  $\eta_{DLA} = 0.9$ ,  $\eta_\kappa = 1$ ,  $\eta = 0.983$ ,  $\eta = 1.04$



Averaged A-type,  $R_p = 4\%$ ,  $R_s = 1.7\%$ ,  $\eta_{DLA} = 0.9$ ,  $\eta_\kappa = 0.997$

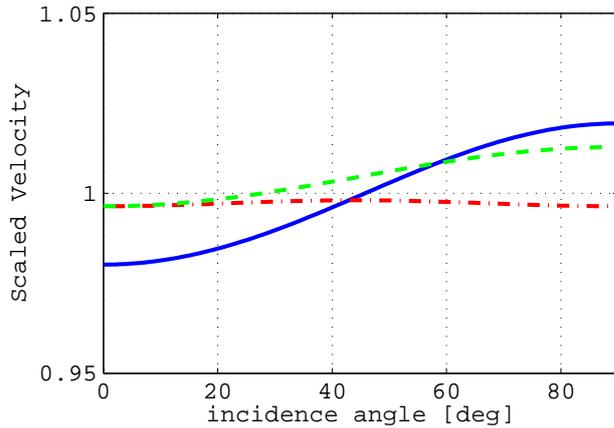


Figure 2: Examples of the incidence angle dependency of bodywaves for the VTI models represented by asterisks in Figure 1. Blue (and magenta in middle) solid lines, red (and cyan) dash-dot lines, and green dashed lines are respectively for  $v_P$ ,  $v_{SV}$ , and  $v_{SH}$ . Phase velocities are scaled by those of corresponding reference isotropic models. (Top), (middle), and (bottom) correspond to the models in (a), (b) and (c) in Figure 1. In the middle panel,  $v_P$  and  $v_{SV}$  shown by magenta and cyan lines are for  $\eta_{DLA} = 1$ ,  $\eta_\kappa = 1.04$  case, and  $v_{SH}$  behaves the same for two cases.